

Observed Seismic Demand on Columns in SCBFs

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Presentation Outline

- Introduction
- Seismic Response of a SCBF
- Effect of Loading Pattern
- Conclusions
- Further Study

Introduction



Fracture progress into column web (FEMA 355E)

ically Braced Fr
become popul



Column flange fracture

(Courtesy of Michael Engelhart, University of Texas, Austin)

Due to the severe damage to SMF SMFs in the 1994 Northridge earthquake, engineers began estimating the material overstrength CBFs.

- Connection details
- On-site welding

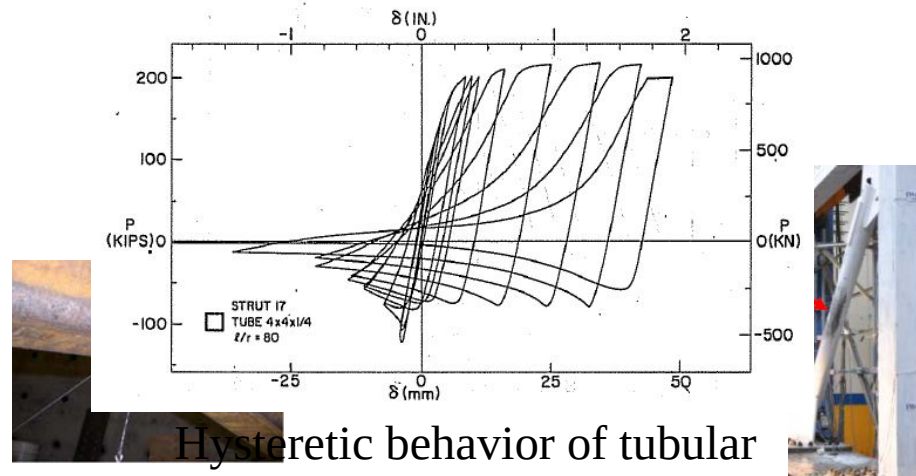
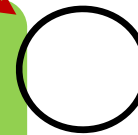
Introduction

What is a CBF?

Two common
shapes for braces



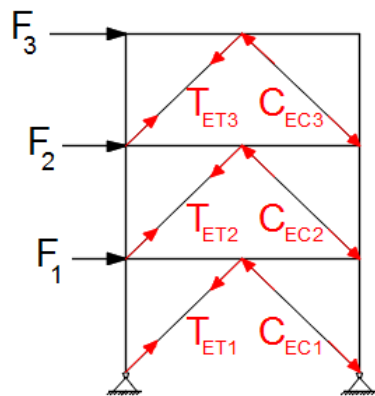
Dissipate EQ
Energy



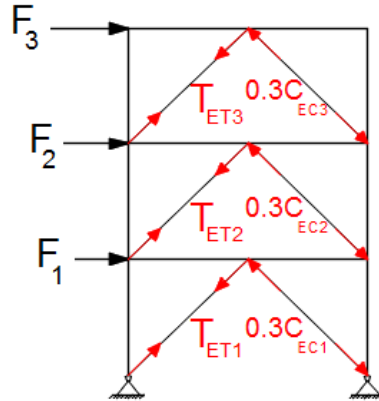
Hysteretic behavior of tubular
bracing (Popov and Black, 1981)
NEES Experimental Test, 2006 Lai & Mahin, 2013

Introduction

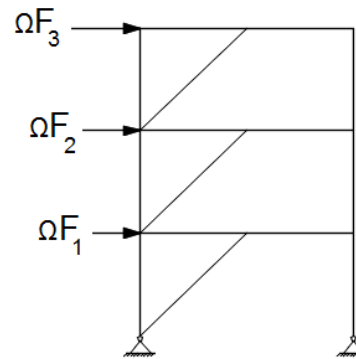
Current design procedure based on AISC 341-10



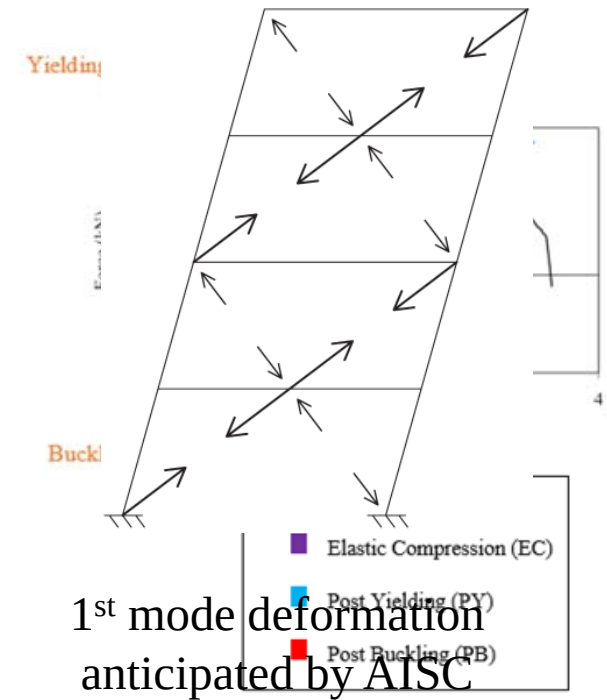
Case I



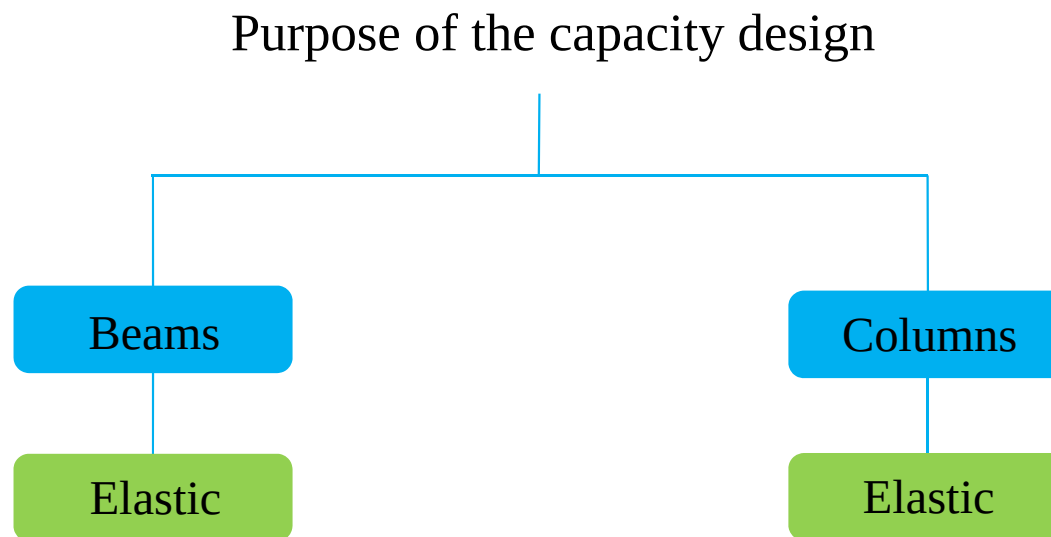
Case II



Case III
(Only for column design)



Introduction

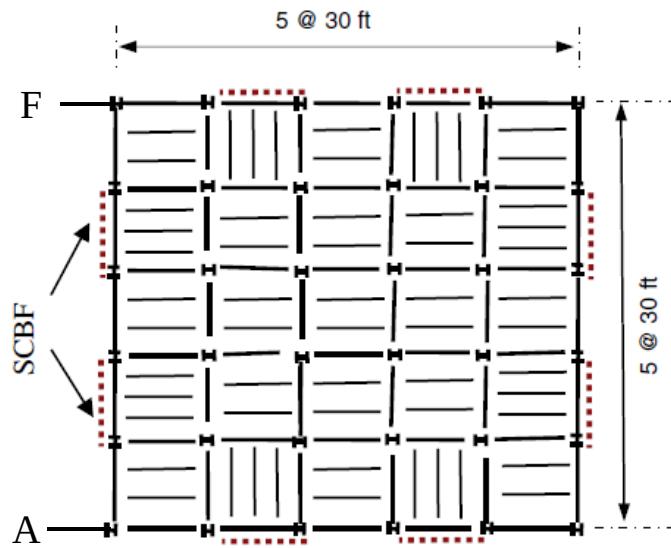


Presentation Outline

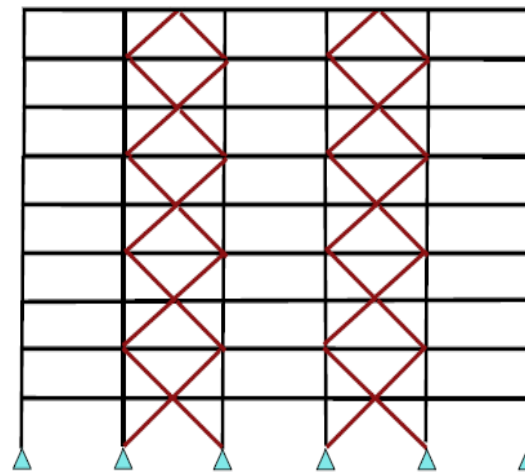
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Seismic response of SCBF

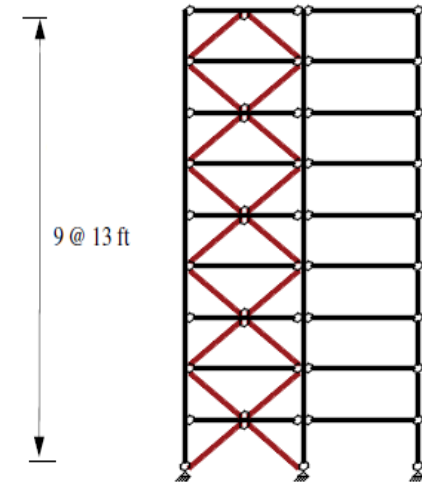
9-Story frame designed based on AISC 341-10



Typical floor plan



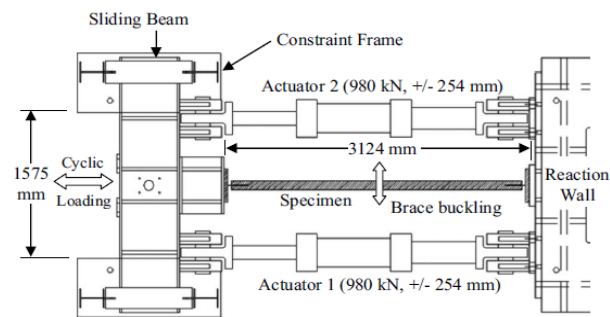
Elevation of Frame A or F



Numerical model

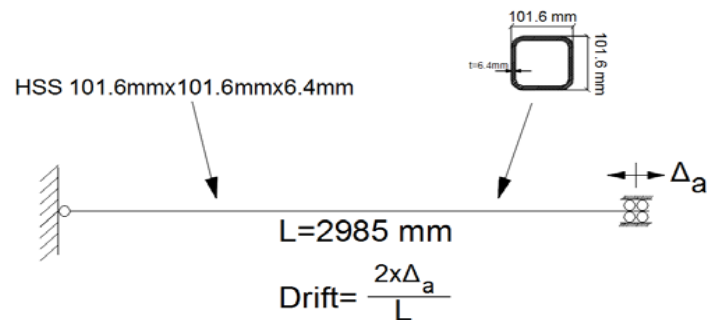
Seismic response of SCBF

Verification:

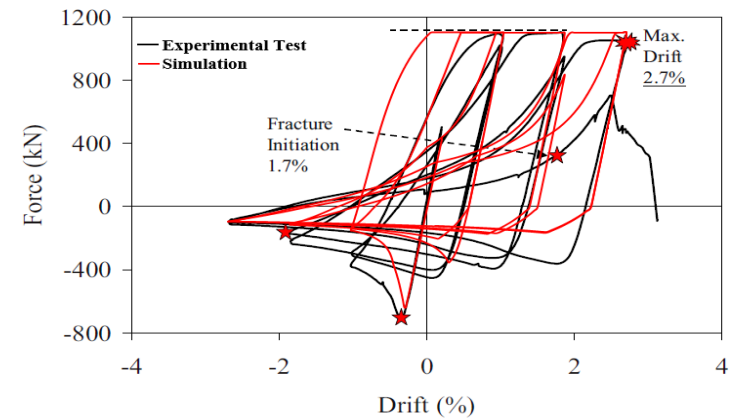


Standard Cyclic		
#cycles	Δ_a (mm)	Drift (%)
6	1.0	0.08
6	1.5	0.10
6	2.3	0.15
4	3.0	0.20 - B
2	15.5	1.03
2	27.9	1.85
2	40.4	2.68
2	59.9	4.00 - MCE
2+n	75.9	5.00

Test setup [Fell et al. (2009)]



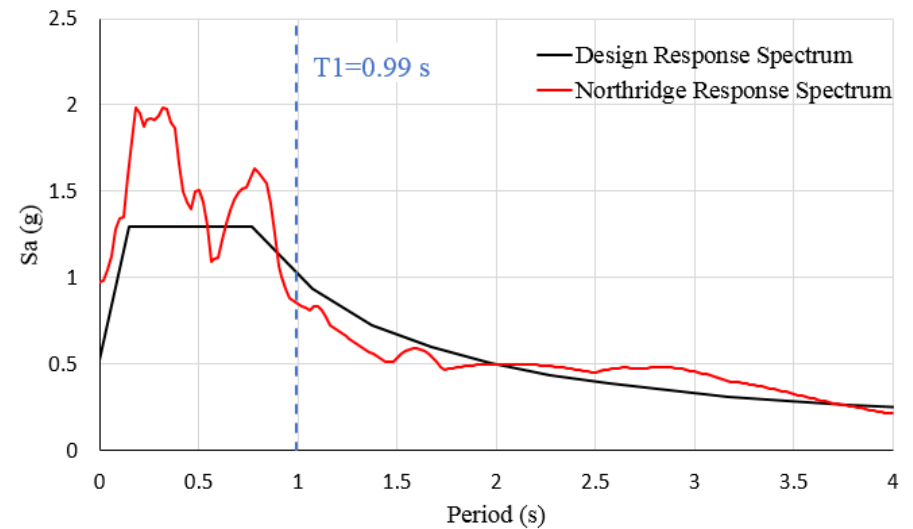
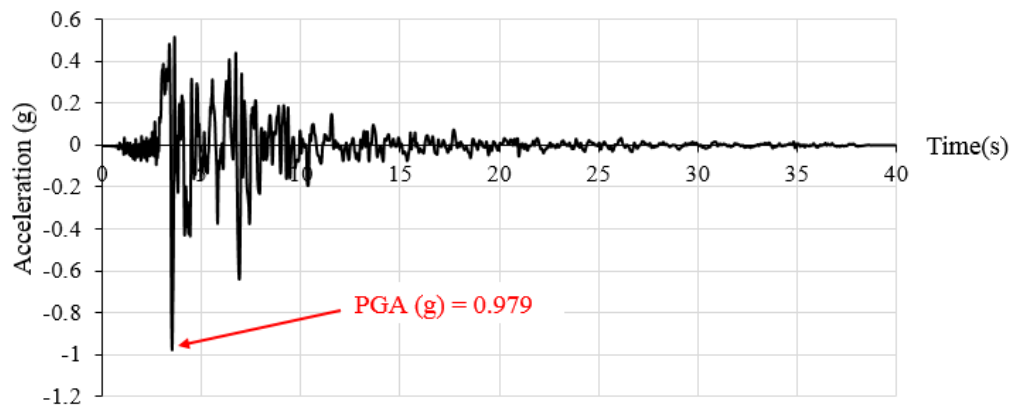
Simulated member



Test and simulation results

Seismic response of SCBF

Ground Motions

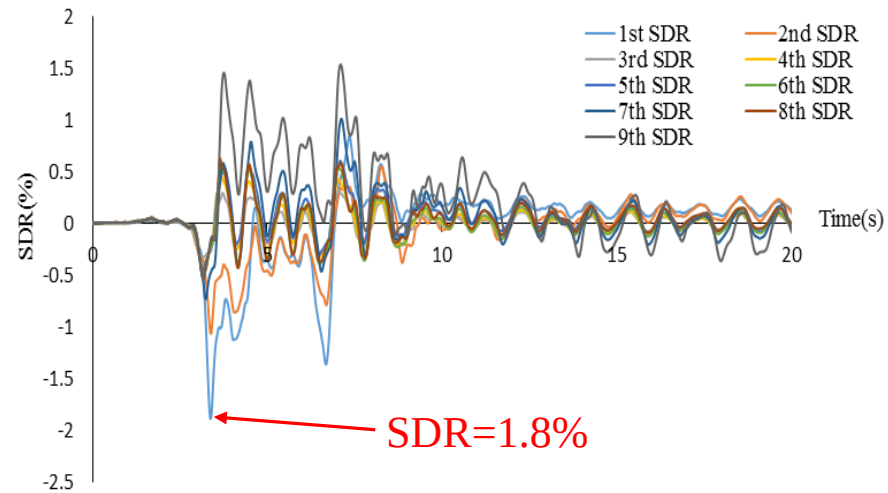


Northridge Ground Motion Specifications

ID no.	NGA#	Sc. factor	Event	Year	Mag	Duration(s)	PGA(g)	PGV(in./s)
GM01	1085	1.1675	Northridge	1994	6.69	40	0.979	53.5

Seismic response of SCBF

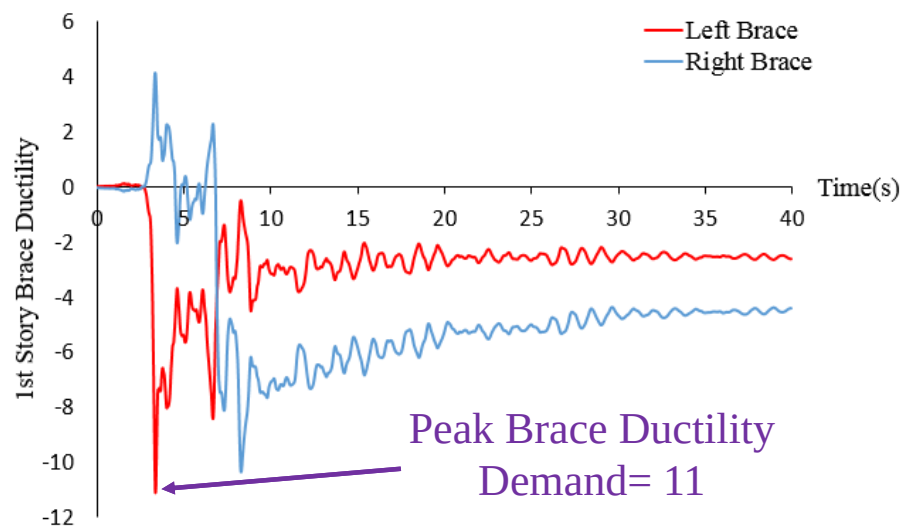
Time history analyses results-Overall response in terms of SDR



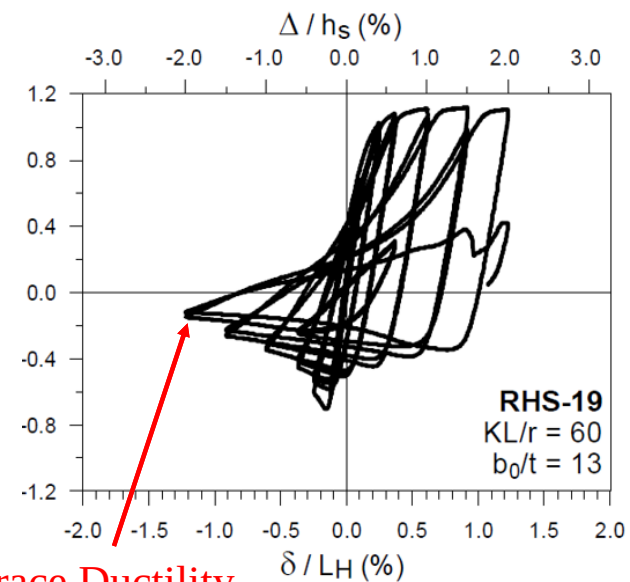
SDR time history under Northridge ground motion

Seismic response of SCBF

Time history analyses results-Brace response



Brace ductility history under
Northridge ground motion



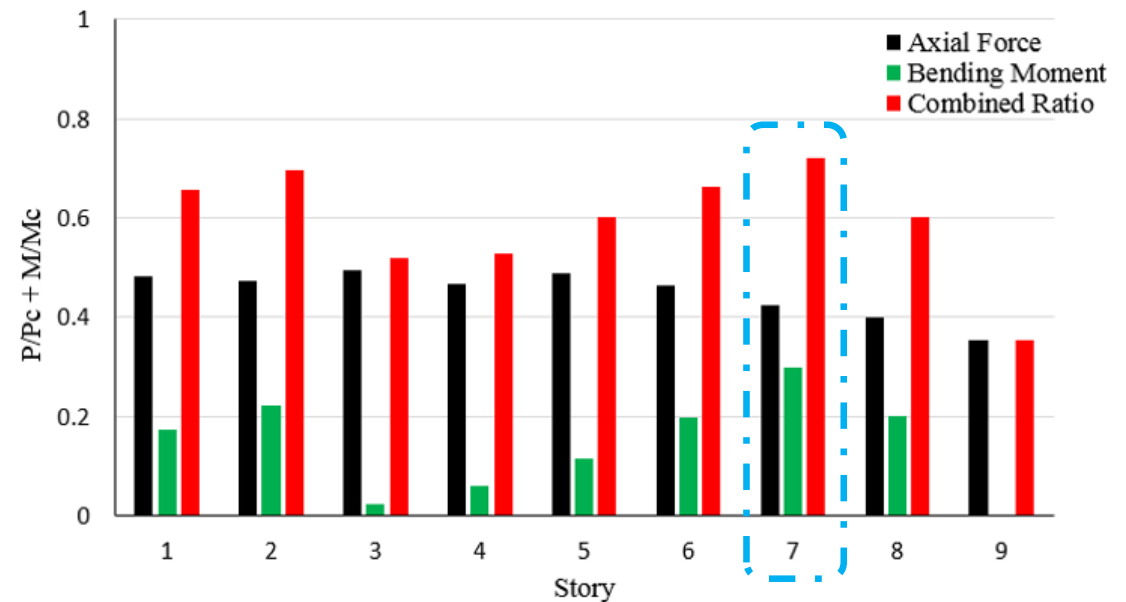
Peak Brace Ductility
Capacity = 8

Experimental Test by Tremblay et al. (2008)

Seismic response of SCBF

Time history analyses results-Column response

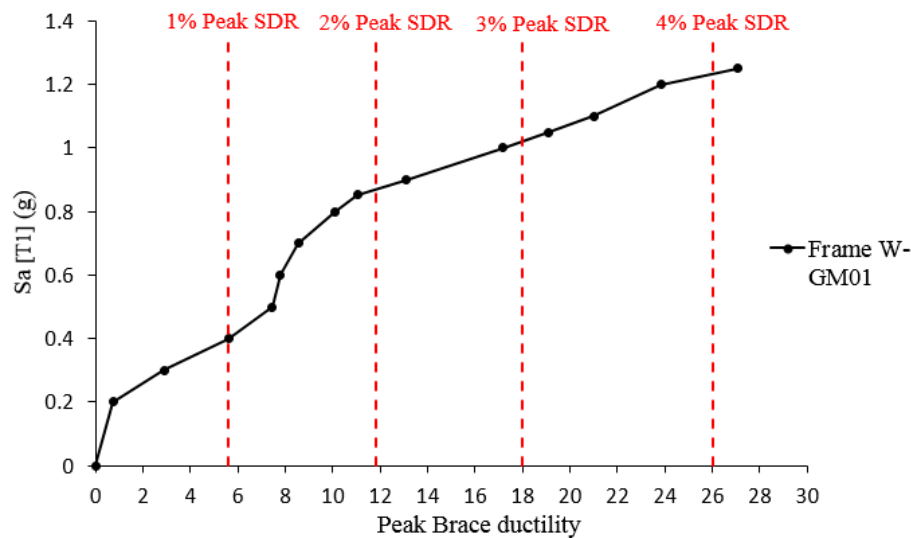
- Flexural demand grows with increasing the SDR of the frame.



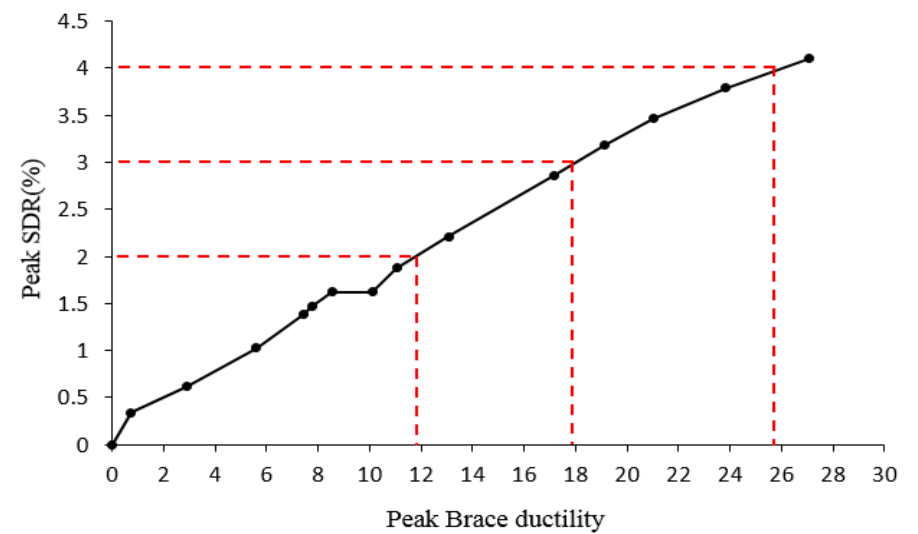
Peak demand on the columns under GM01

Seismic response of SCBF

Incremental Dynamic Analysis (IDA) results



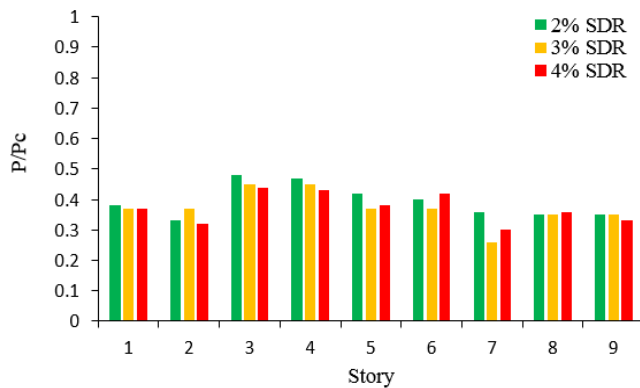
IDA response



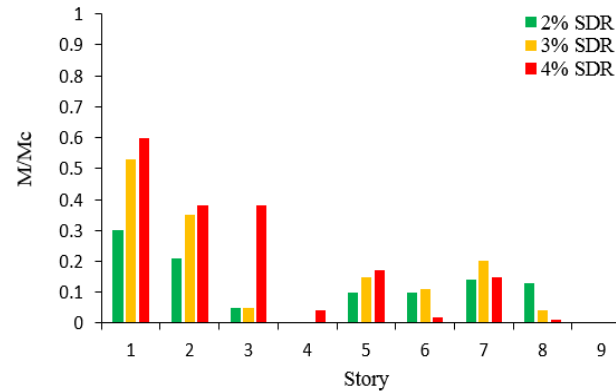
IDA response

Seismic response of SCBF

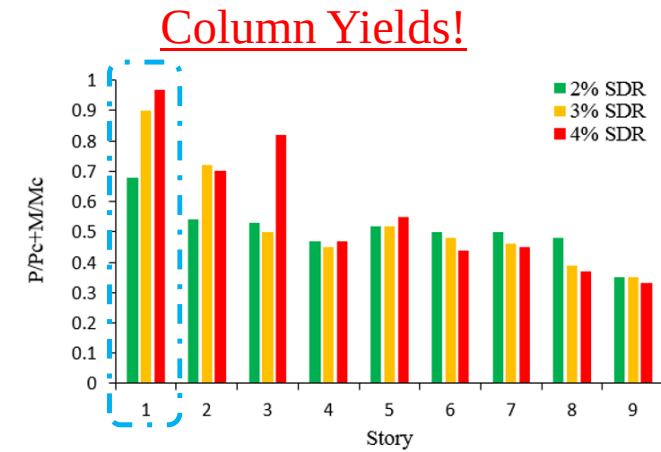
Incremental Dynamic Analysis (IDA) – Column results



Axial force demand/capacity



Flexural demand/capacity



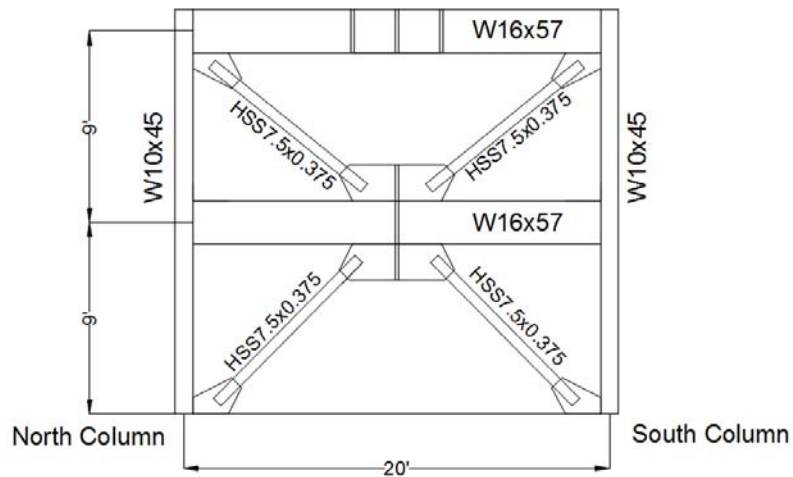
Total demand/capacity

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Effect of Loading Pattern

FEM of TSXBF



Simulated frame in ABAQUS

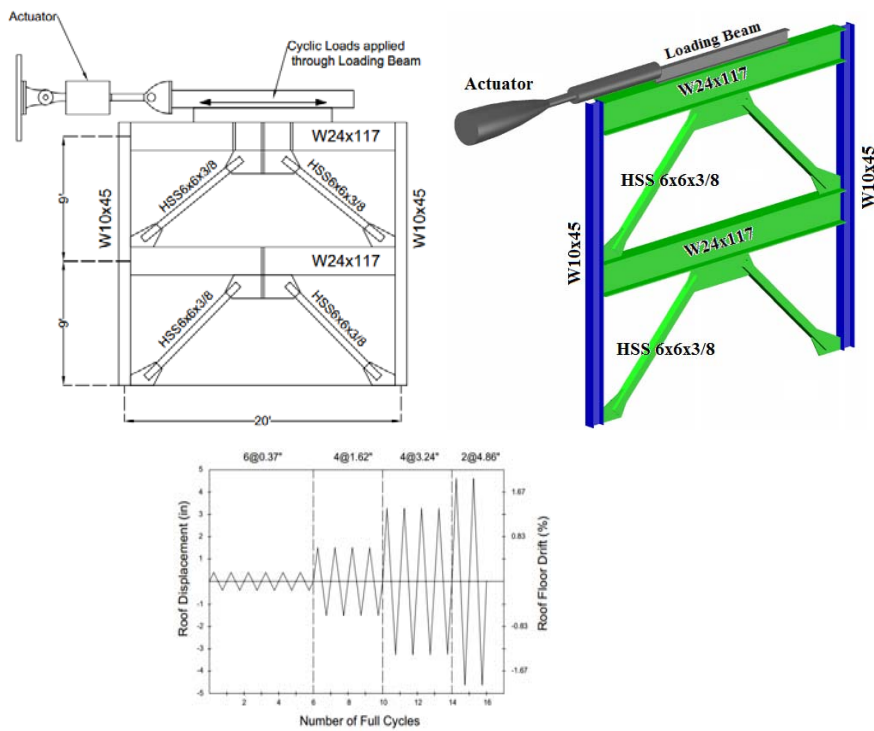
Simulated TSXB Cases

#	Case Name	Frame type	Loading on	Beam size
1	XSM	X-Bracing	Second Story	W16x57
2	XFM	X-Bracing	First Story	W16x57
3	XBM	X-Bracing	Both Stories	W16x57
4	XLBM	X-Bracing	Linear on Both Stories	W16x57

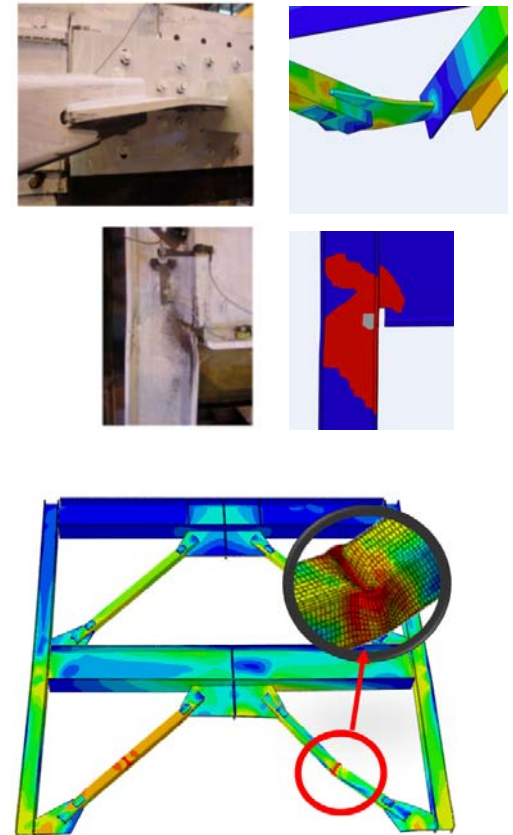
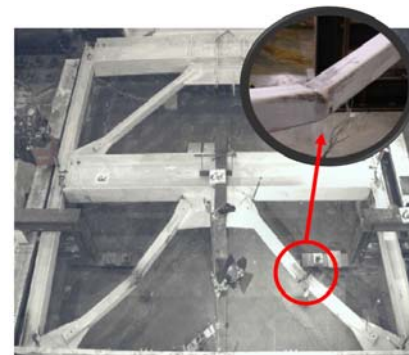
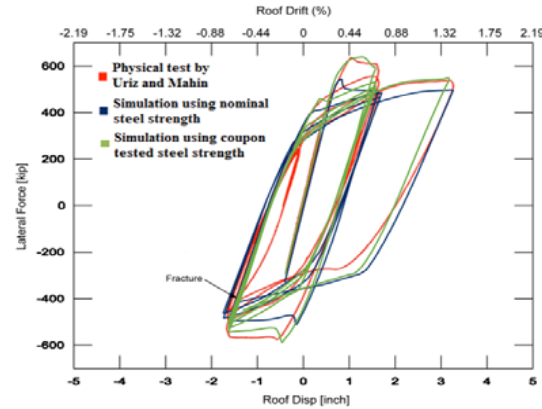
Four loading patterns achieved from dynamic time history analyses results

Effect of Loading Pattern

FE model verification

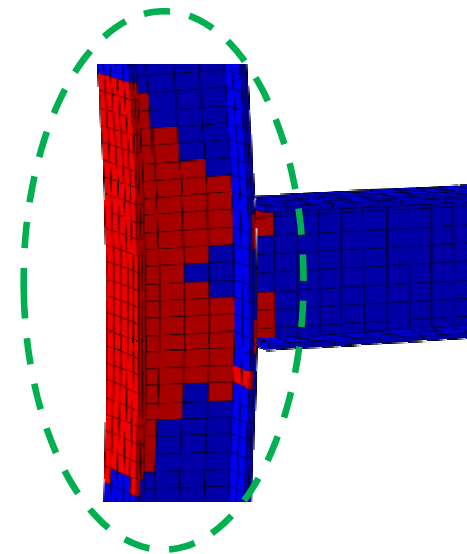
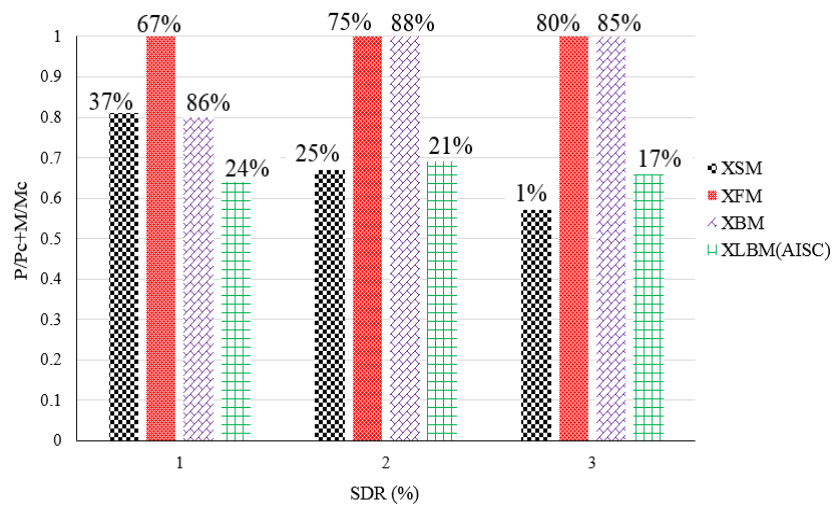


Test setup and loading protocol [Uriz and Mahin, 2001]



Effect of Loading Pattern

FEM results



Column yielded elements in XFM model

Observations:

- Loading pattern suggested by AISC is not necessarily the worst case.
- Higher mode deformation has a significant effect on the demand.

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Conclusions

- **Brace ductility demand** at design drift limit can be **larger than** brace ductility **capacity**.
- **Brace ductility demand** might be **as large as 25** at 4% story drift ratio.
- **Columns** in special concentrically braced frames **experience yielding** which is unexpected.
- **First mode loading pattern is not** necessarily the most **critical pattern** for designing of the two-story X-braced frames.
- Further study needed to evaluate the seismic demand on the columns in SCBFs by using more ground motions and make recommendations to improve the current design procedure if necessary.

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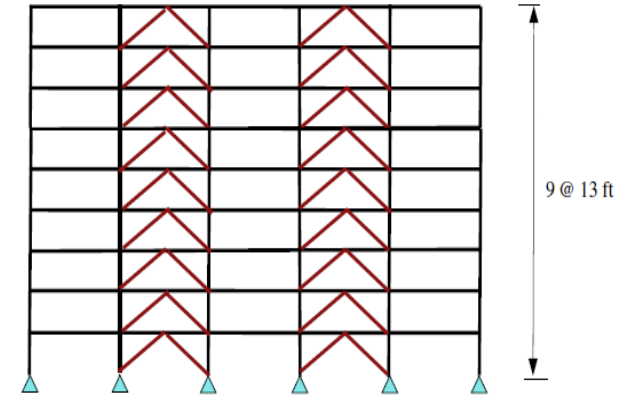
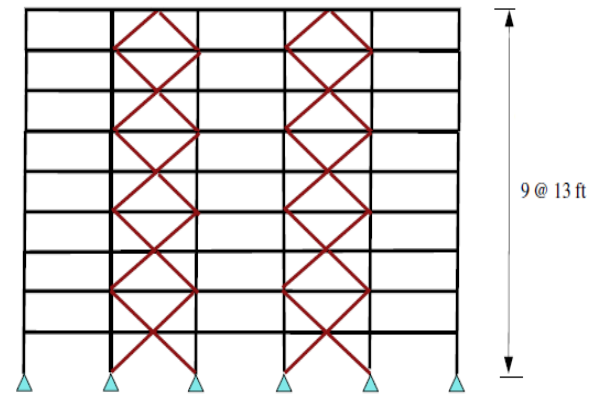
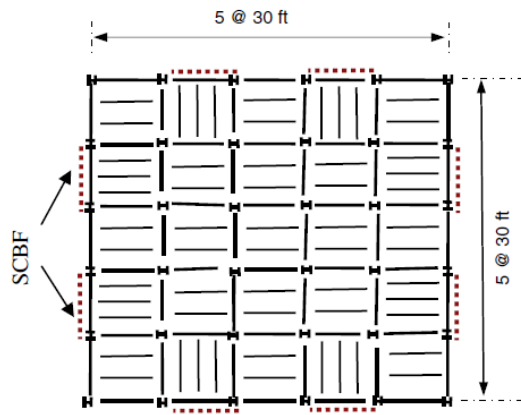
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Further Study

- Seismic performance of concentrically braced frames with and without brace buckling
Engineering Structures
- Seismic demand on brace-intersected beams in two-story X-braced frames
Engineering Structures
- Mechanisms in Two-Story X-Braced Frames
Journal of Constructional Steel Research
- Seismic Performance of All-Steel Buckling-Controlled Braces with Various Cross-Sections
Journal of Constructional Steel Research (under review)

Thank you!

Frame Design



Dead Load= 80 psf

Live Load= 50 psf

$S_s = 2.0$

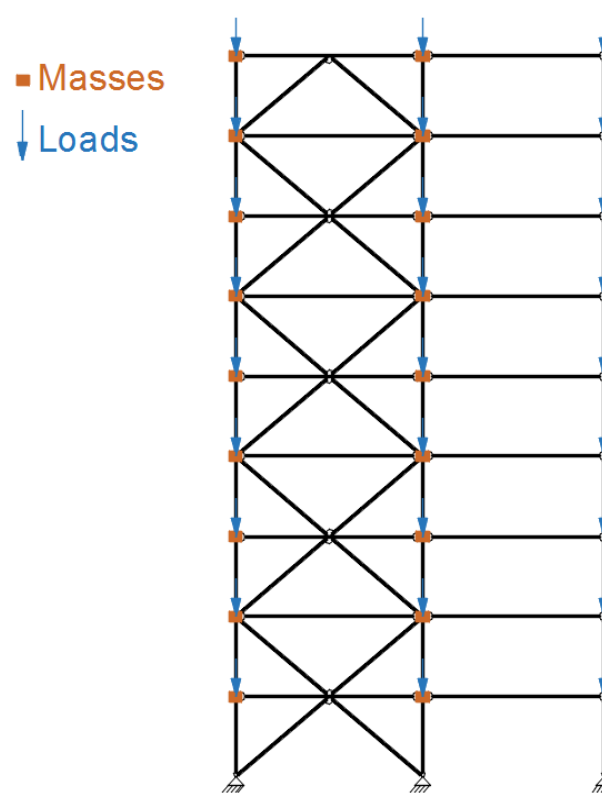
$S_1 = 1.0$

$C_s = 0.22$

Frame Design

Level	Braces	Columns in braced bays	Beams			Gravity Columns	Gravity Beams
			Frame W	Frame S	Frame C		
9	HSS 8.625×0.375 (KL/r = 81, D/t = 24.7)	W14×48	W30×211	W30×211	W30×211	W10×33	W18×65
8	HSS 10×0.625 (KL/r = 71.1, D/t =17.2)	W14×132	W18×86	W18×86	W33×318	W10×33	
7			W18×65	W30×326			
6	HSS 10×10×5/8 (KL/r = 62.5, D/t = 14.2)	W14×233	W21×93	W21×93	W36×395	W10×33	
5			W18×65	W33×387			
4	HSS 14×0.625 (KL/r = 50, D/t = 24.1)	W14×370	W21×111	W21×111	W36×395	W10×33	
3			W18×65	W36×395			
2	HSS 14×0.625 (KL/r = 50, D/t = 24.1)	W14×550	W21×111	W21×111	W36×395	W10×33	
1			W18×65	W36×395			

Seismic Behavior of SCBFs



Loads and masses applied to the simulated frames.

References

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